

# Cryogenic Summary - Testing D2L104 in MAGCOOL, Part I (10/30 – 12/18/2002)

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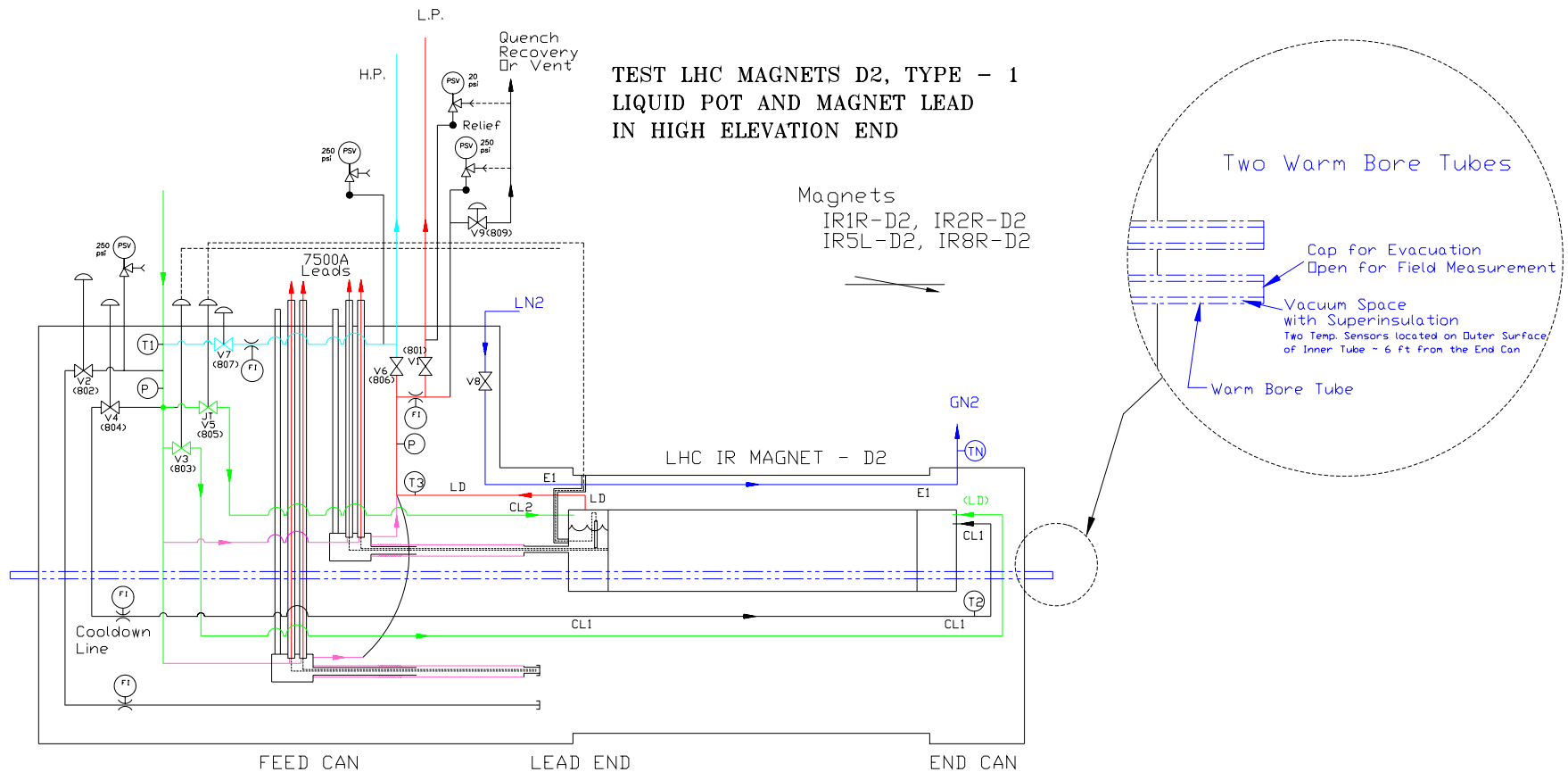
1/11/03

- General Description
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- Summary

# General Description – D2L104

- 0.28 % slope (slightly less than the 0.36 % slope in LHC IR8),
- Warm bore tubes inserted and evacuated
- Information on the Warm Bore Tube and measuring device can be obtained from
  - A. Marone - andym@bnl.gov
  - G. Ganetis – ganetis1@bnl.gov
  - D. Sullivan – dans@bnl.gov

Flow diagram of D2L104 with Warm Bore Tubes –  
Capable of feeding liquid He from either high or  
low elevation ends



# Operating Summary

- 1<sup>st</sup> cooldown (10/3)

Ultem insulator on (+) lead cracked in the beginning of 5 K cooldown. Stop cooldown. Proceed warmup and replace insulator.
- 2<sup>nd</sup> cooldown (11/29)

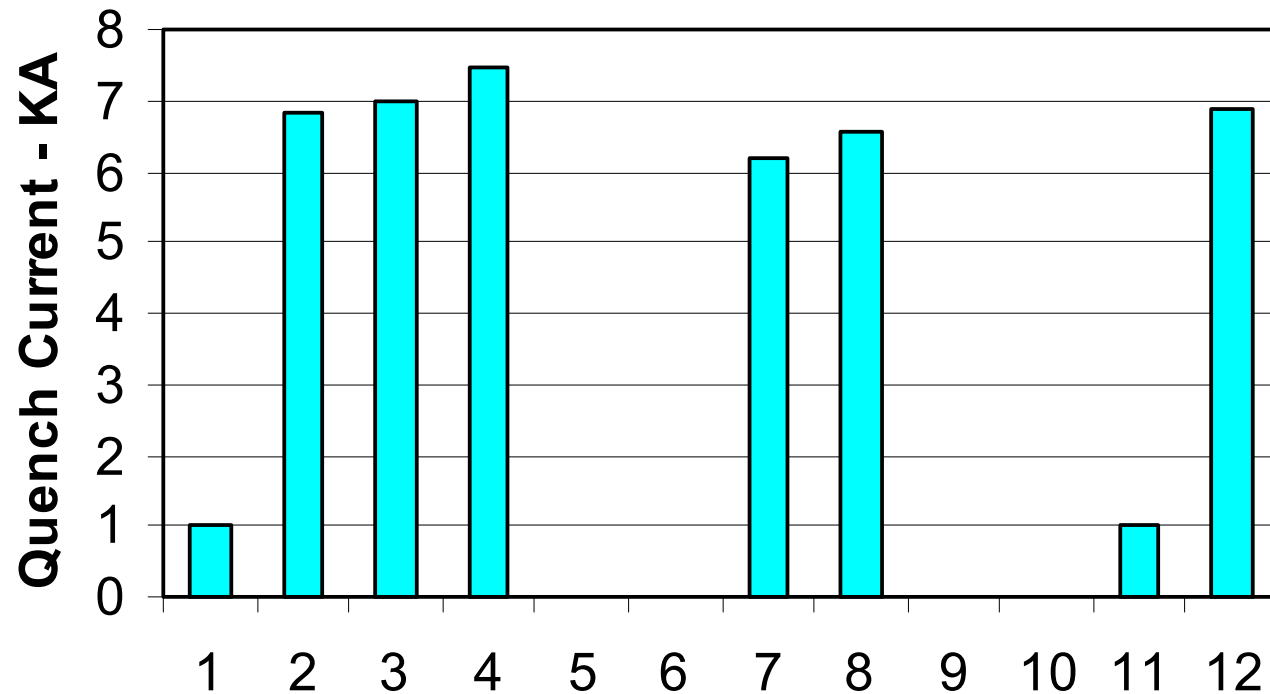
Test D2 in forced flow and liquid. Blockages of flow passage in all 4 leads after a drift in the weekend of 12/7. Proceed warmup to get rid of the contaminants.
- 3<sup>rd</sup> cooldown (12/11)

Test D2 in forced flow after the thermal cycle. Problem occurred on the transformer in B902 substation. Test was cut short due to Christmas holiday. Proceed warmup.

# Quench Performance - D2L104

- 1<sup>st</sup> test group (forced flow cooling  $\sim 4.65$  K),
  - Shut off - 1000 A (12/5)
  - 1<sup>st</sup> quench - 6827 A (12/5)
  - 2<sup>nd</sup> quench - 7001 A (12/6)
  - 3<sup>rd</sup> quench - 7467 A (12/6) (considered as 7500 A)
- 2<sup>nd</sup> test group (liquid cool  $\sim 4.68$  K),
  - 1<sup>st</sup> quench - 6169 A (12/6)
  - 2<sup>nd</sup> quench - 6567 A (12/7)
- 3<sup>rd</sup> test group (forced flow cooling  $\sim 4.59$  K),
  - Shut off - 1000 A (12/16)
  - 1<sup>st</sup> quench - 6890 A (12/16)

# Quench Performance of D2L104 with Warm Bore Tubes Evacuated (1000 A is Shut Off)



Quench - No. 1- 4 (Forced Flow), No. 1 - 1 KA shutoff

No. 7-8, D2L104 (Liquid Cool)

No. 11 - 12, (Forced Flow after Thermal Cycle)

# Operation (10/30 – 12/2)

- 10/30 – 11/2 1<sup>st</sup> time cooldown for D2L104.  
Encountered several equipment failures.  
Took almost 4 days to reach 100 K.  
Approximately 10 minutes after 6 K cooldown began, found the Ultem insulator on (+) lead cracked.
- 11/4 – 20 Proceed warmup and install a new insulator.  
Both warm bore tubes, lead pot window and vacuum vessel were removed and re-installed..
- 11/21 – 27 Warm measurement
- 11/29 – 30 Begin 2<sup>nd</sup> time 100 K Cooldown,  
Rate was slightly slower than 1<sup>st</sup> time
- 12/1 CS5 tripped overnight, restart cooldown
- 12/2 Takes 3 days to finish Cooldown I

# Operation (12/3 – 12/6)

- 12/3 Proceed 100 to 6 K cooldown. Use one expander E19. E20 keeps on tripping and unable to run more than 10 min.
- 12/4 Reached 20 K in the morning or 100 to 20 K in 24 hours. Increase JT flow and started E20 to assist cooldown. After many trips and fix up on E20, we reached 8.5 K in  $\sim 7$  hours. Perform high pot check.
- 12/5 1000 A shut off. 6827 A quench
- 12/6 Warm bore insulating vacuum 0.005 Torr,  
Vacuum inside warm bore  $\sim 0.170$  Torr,  
Insulating vacuum for D2  $< 10^{-6}$  Torr
- 12/6 7001 A, 7469A quenches – considered forced flow cooling complete.



# Operation (12/6 – 12/7)

- 12/6      Switch to liquid cool in  $\sim 30$  min. smoothly,  
It takes  $\sim 2$  hours and not fully cooldown,  
Reach acceptable test condition for liquid mode, 83 %  
liquid level in high end & 89 % in low end.  
Difference  $\sim 6$  % or  $\sim 3$  cm. Agree with slope of  
0.36%. Quenched at 6169 A - surprisingly low.
- 12/7      D2 stay in liquid mode overnight. Auto JT control  
produced oscillation of liquid level between 25 & 45  
%. Manually set JT at 87% to bring liquid level.  
Liquid level 86% and 93% in D2. Tare flow 0.010  
g/s on all 4 leads. Increase Tare flow to 0.17 and 0.32  
g/s for the (+) and (-) leads. Ramp D2. Stay  $\sim 5$  min.  
at 5000 A for the voltage on the (-) lead to decrease.  
Quenched at 6567 A.

# Operation (12/7 - 14)

- 12/7 – 8 Switch to liquid production, leave D2L104 drift
- 12/9 Find blockage of flow passages in all 4 leads during 6 K cooldown, unable to eliminate blockage using local warmup or with warm helium, proceed complete magnet warmup
- 12/10 When return temperature from D2 reached 200 – 210 K, blockage in lead 1 and 2 disappeared.
- 12/11 When return temperature from D2 reached 280 K, blockage in lead 3 and 4 disappeared suggesting the blockage is from water.
- 12/11-12 Perform leak check and proceed 100 K cooldown (3<sup>rd</sup> time cooldown on D2L104).
- 12/13-14 Finish 100 K cooldown in ~ 40 hours.  
Start 5 K cooldown using two expanders. Overnight, refrigerator did not switch into the last by-pass due to minor drifting on the JT setting. Takes ~ 36 hours to finish 5 K cooldown.

# Operation (12/14 – 18)

- 12/14 Perform cold check at  $\sim 10$  K.
- 12/15 Reach 4.6 K test condition – forced flow cooling. Problem on power supply. Unable to ramp.
- 12/16 Problem developed on Transformer in B902 substation. Electrical power to HEUB was off for  $\sim 5$  minutes during diagnosis of Transformer. HEUB was shutdown manually. After temporary power is available, recool D2 to test condition. Perform 1000 A shutoff and 6890 A quench. Warm bore insulating vacuum is believed  $\sim 0.005$  Torr, vacuum inside warm bore  $\sim 0.170$  Torr, Insulating vacuum for D2  $< 10^{-6}$  Torr
- 12/16 Shutdown HEUB after 6890 A quench for transformer work. Leave D2 drifting.
- 12/17 Electrical returned at 9:30. D2  $\sim 31$  K. Insufficient time to cooldown and test before Christmas shutdown.
- 12/18 Proceed warmup.

# Cryogenic Test Conditions

- Forced flow cooling

12 atm, 4.6 K & 65 g/s, magnet temperature  
~ 4.6 K prior to ramp

- Liquid helium cooling

1.49 atm & ~ 4.67 K in D2L104,  
(low temperature portion of MAGCOOL is not  
fully cold, test is performed with JT inlet between  
4.5 K and 4.2 K)

Liquid level in end volume

high elevation end: ~ 86% (12 cm above coil)

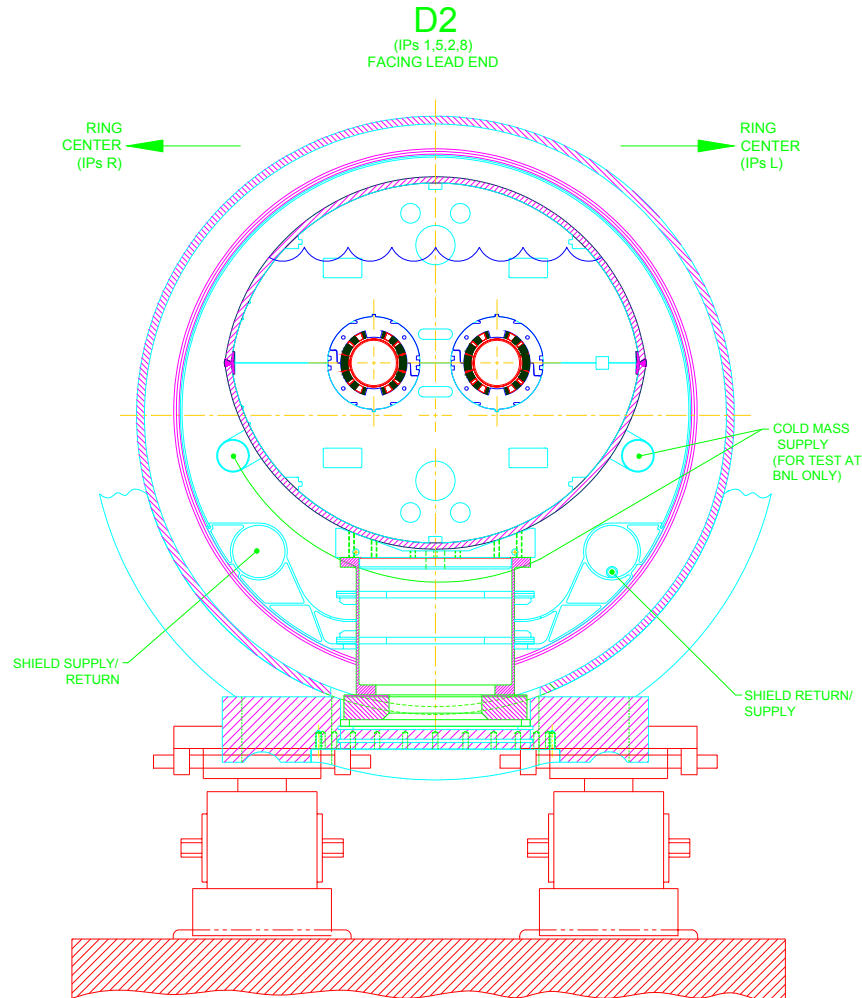
low elevation end: ~ 91% (15 cm above coil)

JT Valve

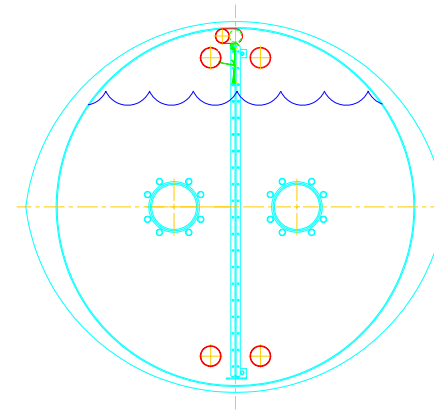
Inlet condition: 11.8 atm & 4.5 K to 4.2 K

Liquid after expansion: ~ 82 % to 89 %

# Sectional View of D2 with Liquid Level in High Elevation End ~ 86% for D2L104 (Left Figure), Level Gauge in End Volume (Right Figure)



Level gauge installed in end volume of D2 cold mass for keeping coil immersed in liquid helium



Shell of cold mass is used as liquid helium vessel with level gauge installed in the end volume for liquid control. For D2L104, liquid is kept at 86 % or ~12 cm above superconducting coil

# Cooldown from 300 – 100 K for D2L104

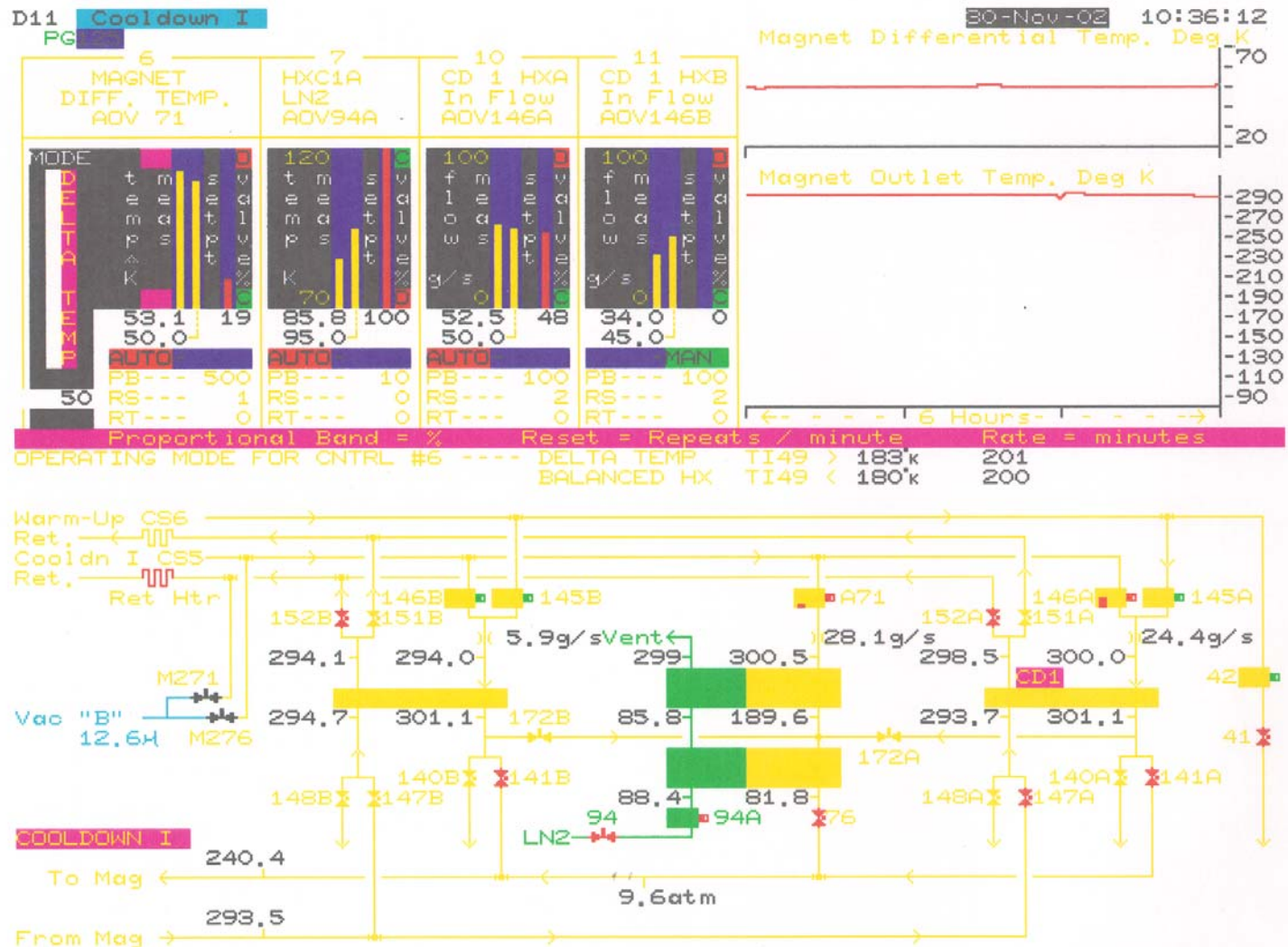
## (11/30-12/3/02)



- 100 K Cooldown time  $\sim$  3 days
- Use 50 g/s of helium flow for MAGCOOL cooldown I on 11/30, cooldown compressor tripped on 12/1, use 60 g/s on 12/2.
- Cooldown rate  $\sim$  2.5 K/hour (11/30),  $\sim$  4 K/hour (12/2)

# Operating Condition for 100 K Cooldown of D2L104

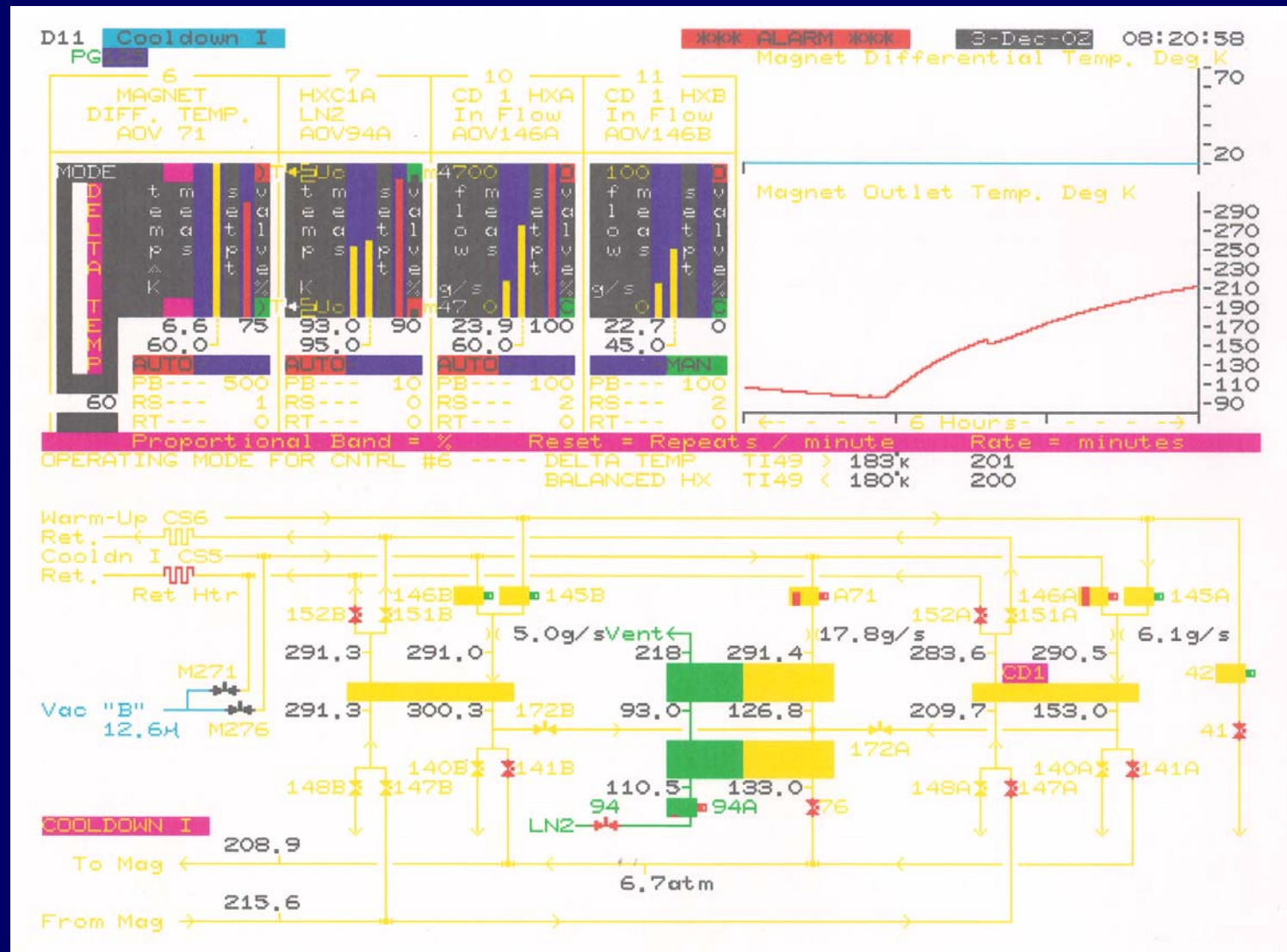
## – 11/30/02 Day 1





# Operating Condition for 100 K Cooldown of D2L104

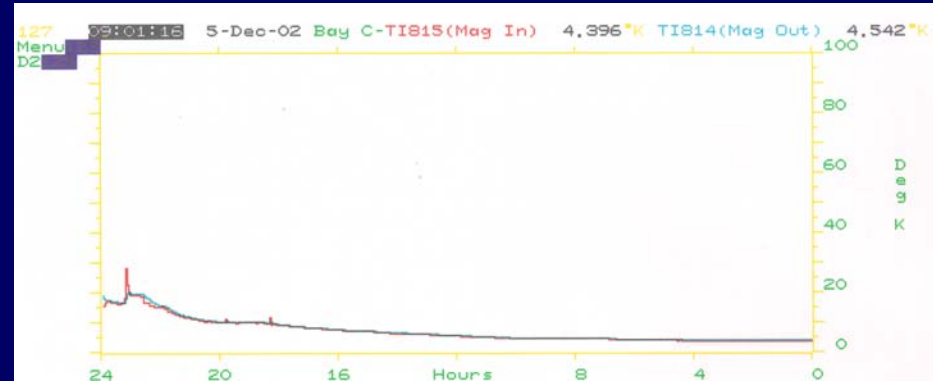
## – 12/3/02 Day 3





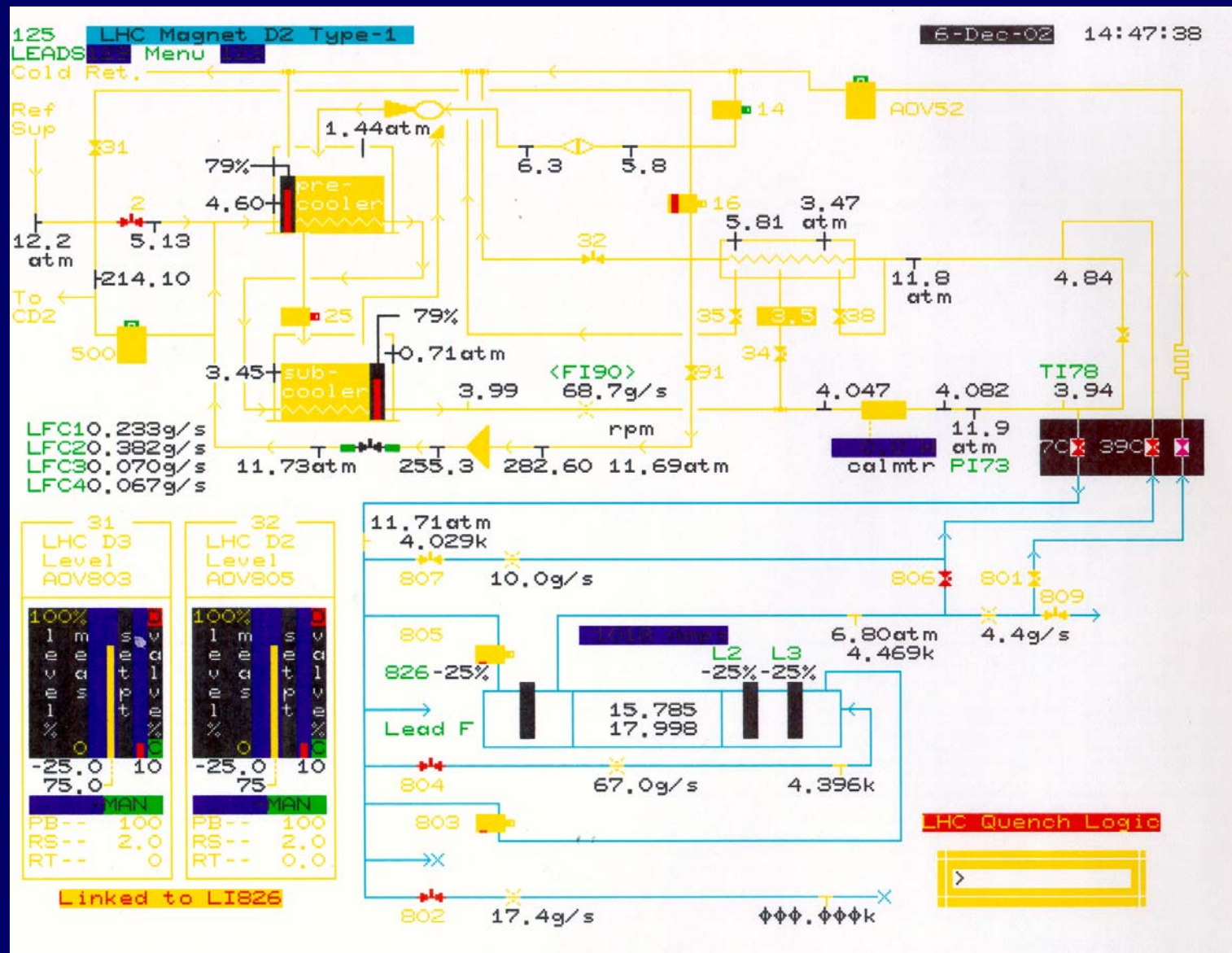
# Cooldown from 100 – 6 K for D2L104

## (12/4 – 5)

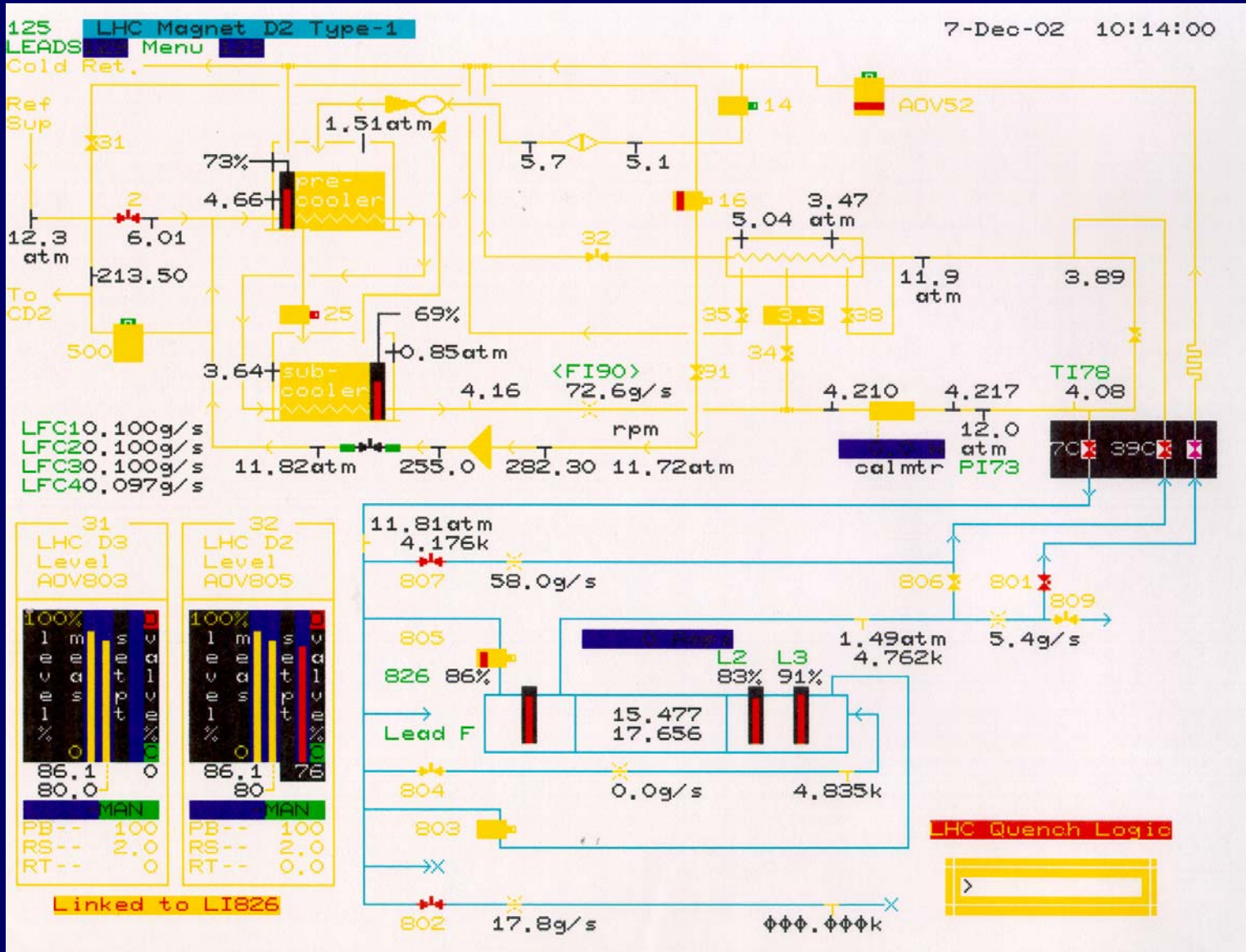


- Cooldown time (100 to 20 K) is 24 hours,  $\sim 3.3$  K/hr, using E19 only
- Cooldown time (20 to 6 K) is  $\sim 8$  hours, 1.8 K/hr, using E19 & E20
- Cooldown time from 20 K to test condition is  $\sim 24$  hours, E19 & E20
- Temperatures at the **inlet (red)** and the **exit (blue)** of D2L104 are shown

# Forced Flow Cooling Condition for D2L104 at 7467 A (Prior to ramping, return temperature is $\sim 4.8$ K in MAGCOOL)

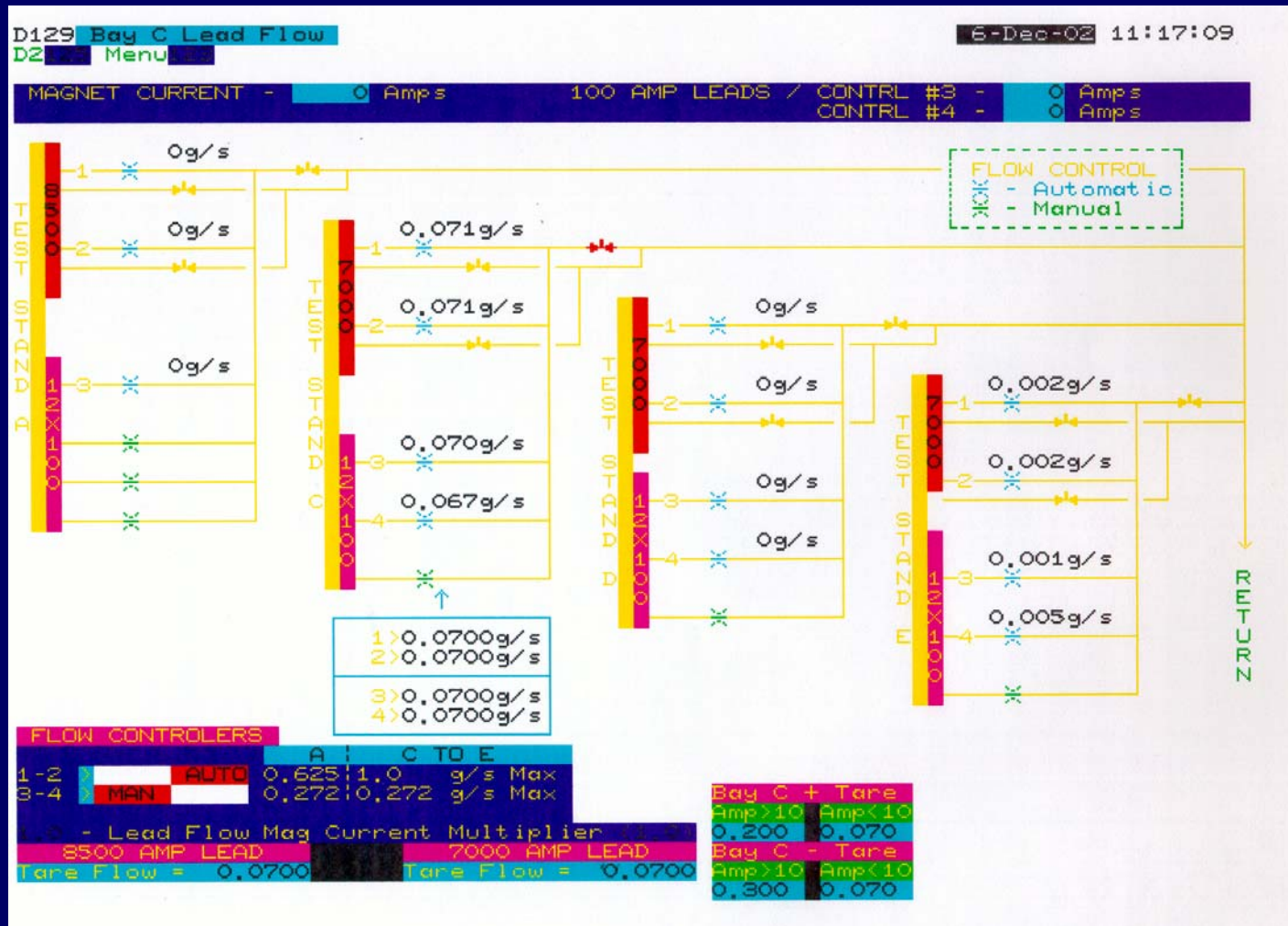


Condition for Ramping D2L104 to 6567 A – Liquid Cool  
(Low temp portion of MAGCOOL was not fully cold)





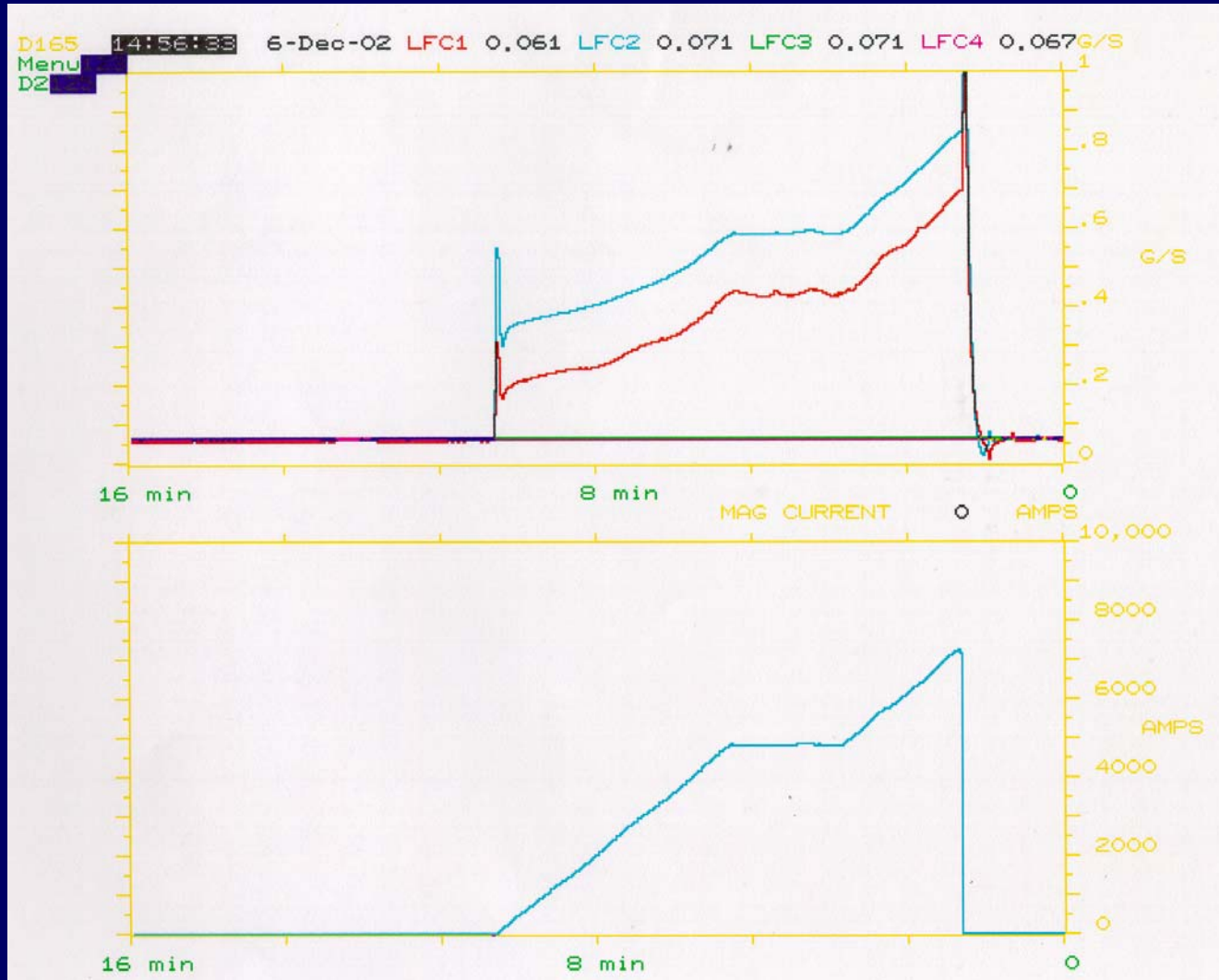
# Separate Flow Control for (+) and (-) Leads in Bay C (Condition for Forced Flow ramping to 7467 A. Need to wait at 5000 A for voltage recovering in the (-) lead.)



# Lead Flow and Current During Ramping of D2L104

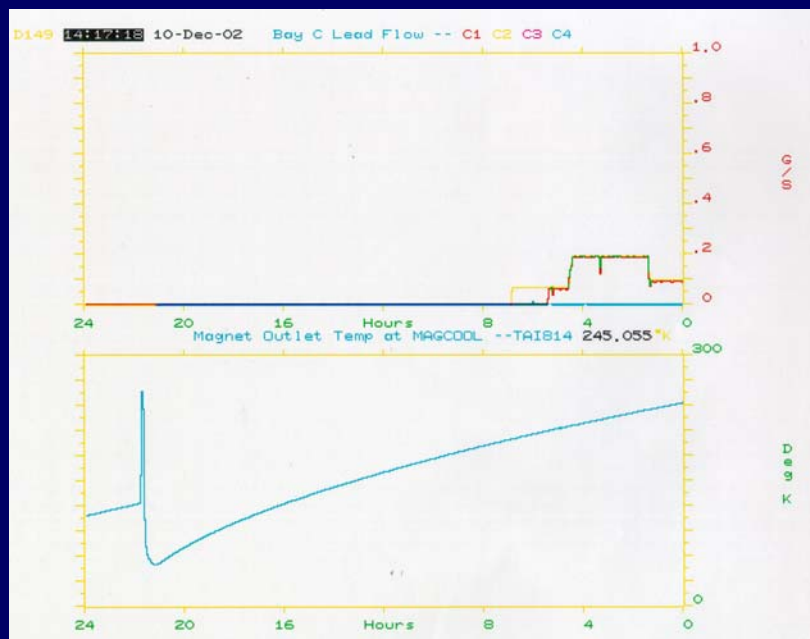
Upper Figure: Lead Flow – Blue for (-) Lead and Red for (+) Lead

Lower Figure: Current as a Function of Time

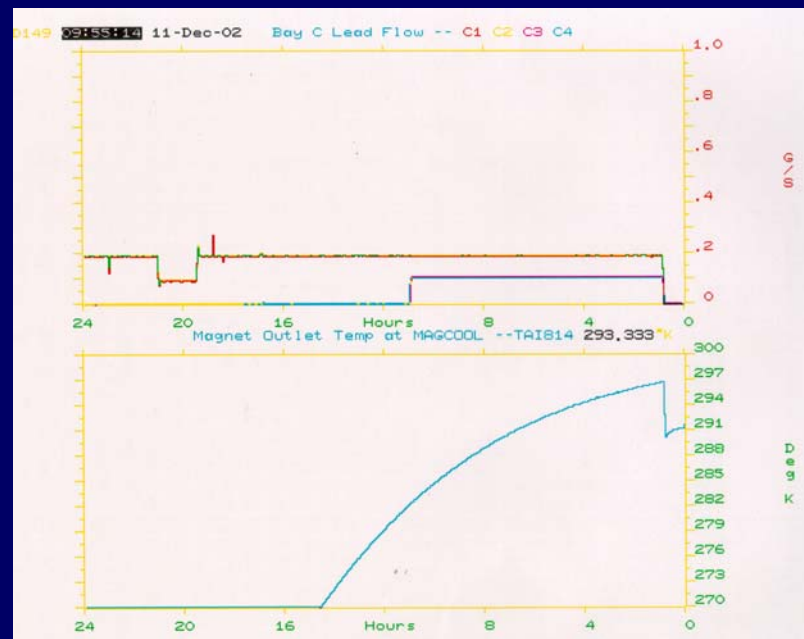


Blockage of Current Leads as Indicated by Lead Flow (upper curve) as a Function of Time. The corresponding temperature exiting D2L104 are given in the lower curve.

Flow is able to pass through lead 1 & 2 when temperature reached  $\sim 210$  K as shown in the left figure. As shown the right, flow is able to pass through lead 3 & 4 when temperature reached  $\sim 280$  K.



No flow is able to pass through lead 1 and 2 until temperature reached  $\sim 210$  K



No flow is able to pass through lead 3 and 4 until temperature reached  $\sim 280$  K

# Lead flow control – for both forced flow and liquid cool

- Main leads
  - Separate flow control for the (+) and (-) leads
  - Tare flow is set at 0.30 g/s for the (-) lead and 0.20 g/s for the (+) lead during ramp up
  - The voltage across the (-) lead is  $\sim 0.055$  V at 7467A
- Unused leads
  - $\sim 0.070$  g/s for the tests

# Summary

- D2L104 is the 1<sup>st</sup> D2 magnet with two warm bore tubes installed for field measurement.
- In the Part I tests, both warm bore tubes were evacuated.
- Many unexpected equipment failure and difficulties were encountered in the two months test period.
- Performance of D2L104 is not as satisfactory as that of D2L102 or D2L103.
- The 3<sup>rd</sup> quench occurred at 7467 A using forced flow cooling with the magnet at  $\sim 4.65$  K.
- Quench currents are lower using liquid cool.
- After thermal cycle, the 1st quench is at 6890 A in forced flow.
- Lower quench currents using liquid helium cool are believed related to warm bore tubes. Unfortunately, the best way to prove is to re-do test with warm bore tubes removed.
- Test will resume in January 2003.